



Memorandum

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Subject: Cascade Noise Analysis of Band 6 Cartridge

1. Summary

A previous memo¹ showed that the gain slope of the Band 6 cartridge can be improved significantly with an equalizer integrated into the warm IF amplifier. To meet both gain slope as well as total power specifications, the equalizer requires the specifications given in Table 1. These are based on discussions with the current vendor, AML Communications, for modifying their warm IF amp to include an amplitude equalizer.

To confirm that these gain values don't degrade receiver noise temperatures, this memo analyses noise temperatures of the cascade consisting of the cold cartridge, warm IF amps, IF switch, and back end. The sensitivity of receiver noise temperature to changes in subsystem parameters is also analyzed.

Table 1: Specifications Assumed for Warm IF Amp with Integrated Equalizer	
Parameter	Value
Gain	22 dB @ 4 GHz 34 dB @ 12 GHz
Noise Figure	2 dB
VSWR	Input: 1.8:1 Output: 1.33:1

Receiver noise temperature is sensitive to the noise figure of the warm IF amps but relatively insensitive to the gain of the IF amps.

2. Cascade Analysis

Bob Freund's noise analysis spreadsheet was modified to perform the analysis here, and sections of the modified spreadsheet are shown in Table 2, Table 3, and Table 4. Figure 1 shows Freund's block diagram modified to include the current IF switch implementation. Freund's spreadsheet was chosen because it includes the ability to calculate performance over a number of IF's, which is useful because it can accommodate gain slope.

Overall cartridge gain was measured by differencing system noise power when the receiver is connected to hot and cold loads and dividing by the difference in the hot and cold load physical temperatures. This is the standard "ΔP/ΔT" technique and implementation details for the Band 6 cartridge are given on ALMA EDM². Gain of just the cold cartridge, shown in Figure 2, is calculated by subtracting from the overall cartridge gain the gain of the warm IF system, which was measured using a network analyzer. For reference, Figure 2 includes the gain of the

¹ "Band 6 Cartridge Power Density Slope Correction Using Warm IF Amps", FEND-40.02.06.00-098-A-DSN, 2006-06-01, available on ALMA EDM at <http://edm.alma.cl/forums/alma/dispatch.cgi/iptfedocs/docProfile/102197>.

² "Band 6 Cartridge Test Procedure Noise Performance, Gain, and Gain Slope," FEND-40.02.06.00-076-A-PLA, 2006-04-26, <http://edm.alma.cl/forums/alma/dispatch.cgi/iptfedocs/docProfile/101778>

relevant mixer-preamp measured using the Mixer Test System, which was also calculated from the “ $\Delta P/\Delta T$ ” technique.

The noise temperature of the mixer-preamp was set in the spreadsheet Table 4 (*Amp D NT D*), to the mixer’s specification values of 136K at 4 and 12 GHz and 83K elsewhere. The input parameter for cold cartridge gain (*Amp D Gain G D*, Table 4) was adjusted so that the cartridge gains calculated in the spreadsheet (*Cold Cartridge Gain*, Table 4) equaled the gains measured in Figure 2.

The warm IF amp parameters are entered in Table 3 at rows *Amp C NT (Warm IF Amp)* and *Amp C Gain (Warm IF Amp)*. Cable attenuation for the warm IF plate was measured on a network analyzer and is entered in Table 3 as *Cable d loss Ld at freq* and *Cable c loss Lc at freq*.

The IF switch was configured for worst-case with its variable attenuator set for 15 dB.

Receiver noise temperature in excess of the mixer-preamps’ noise temperature is called *2nd Stage Noise Contribution* in the spreadsheet and is calculated in Table 2.

3. Noise Temperature Sensitivity Results

Noise temperature sensitivity, shown in Figure 3, is the difference in receiver noise temperature when various subsystem parameters are changed. Note that for a well-designed receiver, the receiver noise should be dominated by the first stage noise temperature with insignificant noise contribution from latter stages. For the Band 6 Cartridge with nominal component values, the noise temperature contribution of latter stages (called *2nd Stage Noise Increase* in the figure) is 0.7K at 6 GHz and 1.7K at 10 GHz.

Figure 3 shows receiver noise temperature is most sensitive to changes between the mixer-preamp and the warm IF amps as shown when either “Pad H” or “Pad F” are increased by 1 dB. Pad H is the 2 dB cold attenuator installed in the 4K stage to reduce ripple. Pad F isn’t actually present, but shows that the receiver noise temperature is sensitive to input cable loss and the noise figure of the warm IF amps.

Receiver noise temperature is relatively insensitive to the gain of the Warm IF amps, the noise figure of the IF switch (Pad B), and the attenuator in the IF switch.

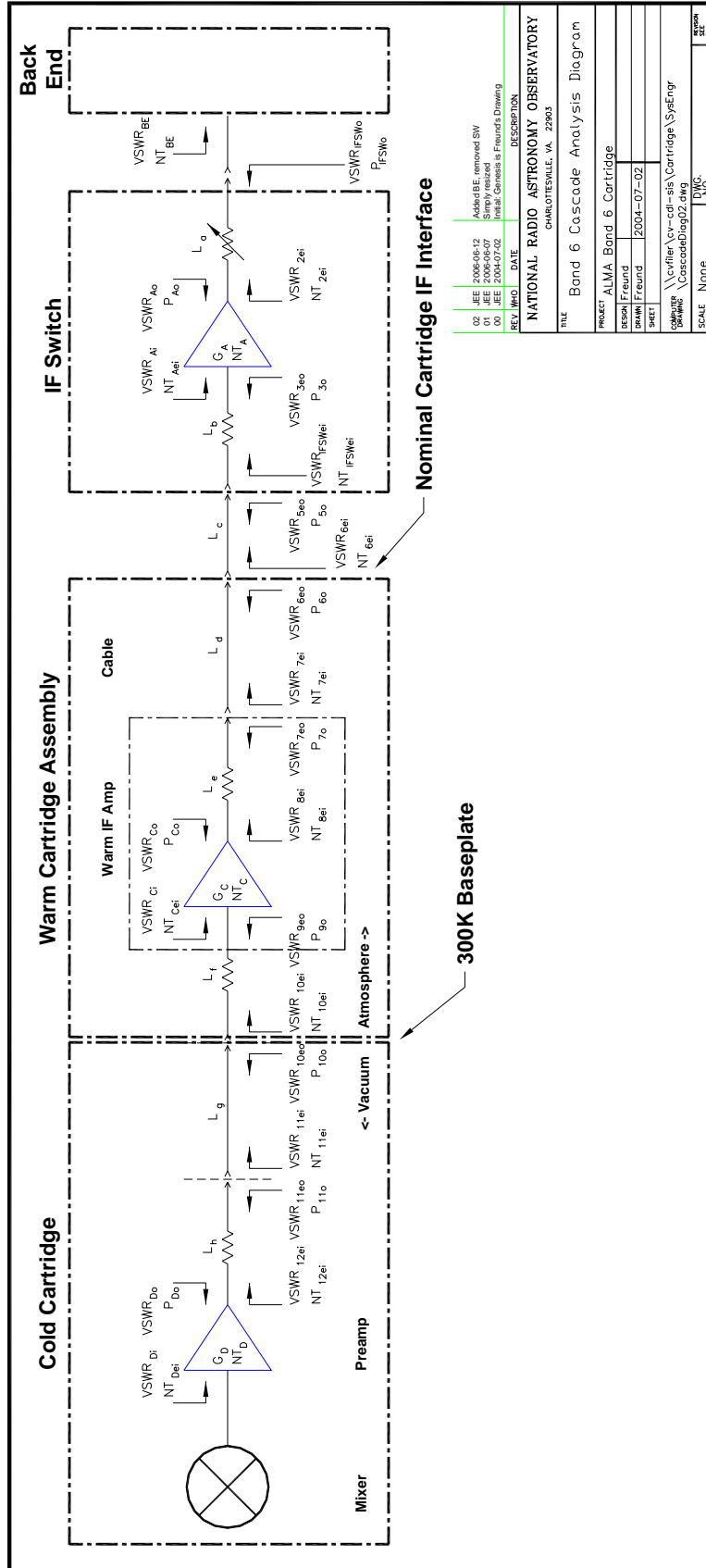


Figure 1: Block diagram of components used in cascade analysis

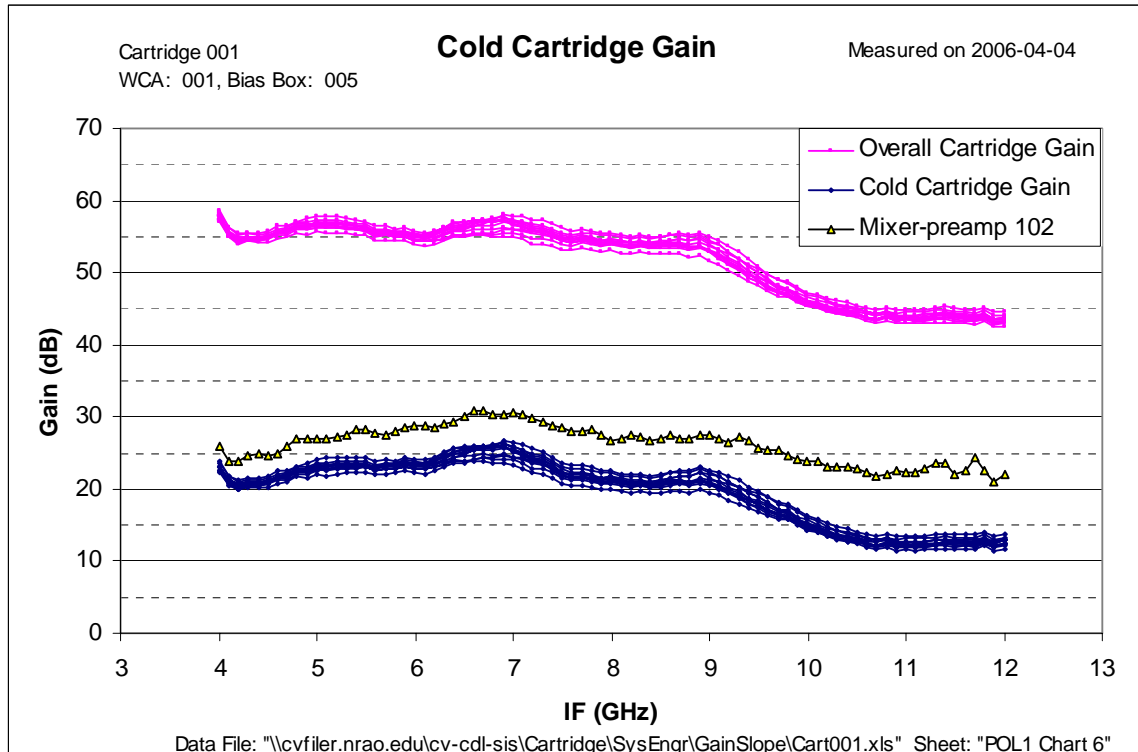


Figure 2: Measured Gain of Overall and Cold Cartridge Compared to Measured Mixer-preamp Gain

	A	B	C	D	E	F	G	H	I	J
1	Front End Signal Path Budget									
2	Version 1 - 2: Bob Freund									
3	Version 3: 2004-03-01 jee changed preamp gain from 30 to 20 dB and noise temp from 34K to 63K so Amp D Effective NT = 77K									
4	Version 4: 2004-07-02 jee changed warm IF amp: NT from 150 to 120K, changed Le to 3 dB (to improve output VSWR)									
5	Version 4.1 2004-08-24 jee added cell for Warm IF NF to NT conversion.									
6	Version 4.2 2004-10-27 Fixed total ripple calculation to include gain slope plus ripple, changed preamp VSWR from 2:1 to 2.46:1, reduced warm IF ripple to 2 dB/2GHz									
7	Version 4.3 2006-06-07 jee added measured SS coax data and changed Warm IF NF to 2 dB									
8										
9	<i>k</i>	1.38E-23								
10	<i>T</i>	300 K								
11	<i>T for 4K Attn</i>	4 K								
12	BW_Full	8.00E+09 Hz								
13	BW_Seg	2.00E+09 Hz								
14										
15	Maximum output power per 2 GHz banc	-27.0 dBm								
16							10	31		
17	Input power over full 8 GHz band	3.31E-11 W		-74.80 dBm						
18	Output power over full 8 GHz band	3.54E-06 W		-24.51 dBm						
19										
20										
21	Freq		4	6	8	10	12	GHz		
22										
23	Total gain		44.13	48.93	51.77	50.62	51.49	dB		
24	Excess gain		-9.69	-4.89	-2.05	-3.20	-2.33	dB		
25										
26	RSS ripple		1.47	1.45	1.44	1.43	1.41	dB pk-pk		
27										
28	Achieved noise temperature		137.6	83.8	83.7	84.7	138.5	K		
29	Second stage noise contribution		1.6	0.8	0.7	1.7	2.5	K		
30										
31										
32	Back End Input NT BE	15 dB <- NF of BE	8,881	8,881	8,881	8,881	8,881	K		
33	Back End Input VSWR BEi	1.40	1.40	1.40	1.40	1.40	1.40			
34	Back End Input Gamma BEi		0.167	0.167	0.167	0.167	0.167			
35										
36	IF SW to Back End Ripple		0.03	0.03	0.03	0.03	0.03	db pk-pk		
37										
38	IF SW Output effective gamma IFSWo		0.011	0.011	0.011	0.011	0.011			
39	IF SW Output effective VSWR IFSWo		1.02	1.02	1.02	1.02	1.02			
40	IF SW Integrated Output Power P IFSWo									-24.5 dBm
41	IF SW Output Power P IFSWo		-36.7	-31.9	-29.1	-30.2	-29.3	dBm		
42	Pad a Maximum Loss La	15.0 dB	15.0	15.0	15.0	15.0	15.0	dB		
43	Pad a effective Input NT _{2ei}		290,016	290,016	290,016	290,016	290,016	K		
44	Pad a Input effective VSWR _{2ei}		1.01	1.01	1.01	1.01	1.01			
45										
46	Amp A Output VSWR _{Ao}	2.0	2.00	2.00	2.00	2.00	2.00			
47	Amp A Integrated Output Power P _{Ao}									-9.5 dBm
48	Amp A Output Power P _{Ao}		-21.7	-16.9	-14.1	-15.2	-14.3	dBm		
49	Amp A Gain G _A	15.0 dB	15.0	15.0	15.0	15.0	15.0	dB		
50	Amp A NT _A (NF IF Switch)	15.0 dB	8,881	8,881	8,881	8,881	8,881	K		
51	Amp A effective NT _{Aei}		18,052	18,052	18,052	18,052	18,052	K		
52	Amp A Input VSWR _{Ai}	2.0	2.00	2.00	2.00	2.00	2.00			
53										

Table 2: Spreadsheet 1

	A	B	C	D	E	F	G	H	I	J
54	Pad b Output effective VSWR _{3eo}			1.28	1.27	1.26	1.26	1.25		
55	Pad b Integrated Output Power P _{3o}									-24.5 dBm
56	Pad b Output Power P _{3o}			-36.7	-31.9	-29.1	-30.2	-29.3 dBm		
57	Pad b Loss L _b	0.0 dB		0.0	0.0	0.0	0.0	0.0 dB		
58	IFSW effective Input NT _{IFSWei}			18,052	18,052	18,052	18,052	18,052 K		
59	IF SW Input effective VSWR _{IFSWei}			2.00	2.00	2.00	2.00	2.00		
60	IF SW Input effective gamma _{IFSWei}			0.333	0.333	0.333	0.333	0.333		
61										
62	Cartridge Interface with IF cables and switch									
63										
64	Cable c Output effective VSWR _{5eo}			1.28	1.27	1.26	1.26	1.25		
65	Cable c Integrated Output Power P _{5o}									-24.5 dBm
66	Cable c Output Power P _{5o}			-36.7	-31.9	-29.1	-30.2	-29.3 dBm		
67	Cable c loss L _c	76.2 dB per 100 ft		0.29	0.36	0.42	0.47	0.51 dB		
68	at freq	18.0 GHz								
69	Cable c length	0.25 m								
70	Cable c NT _c			21.1	26.0	30.2	34.0	37.4 K		
71	Cable d Input effective NT _{5ei}			19,340	19,642	19,900	20,130	20,341 K		
72	Cable d Input effective VSWR _{5ei}			1.905	1.885	1.869	1.855	1.842		
73										
74	Cable d Output effective VSWR _{6eo}			1.31	1.30	1.30	1.29	1.29		
75	Cable d Integrated Output Power P _{6o}									-24.1 dBm
76	Cable d Output Power P _{6o}			-36.4	-31.5	-28.6	-29.7	-28.8 dBm		
77	Cable d loss L _d	76.2 dB per 100 ft		0.29	0.36	0.42	0.47	0.51 dB		
78	at freq	18.0 GHz								
79	Cable d length	0.25 m								
80	Cable d NT _d			21.1	26.0	30.2	34.0	37.4 K		
81	Cable d Input effective NT _{7ei}			19,340	19,642	19,900	20,130	20,341 K		
82	Cable d Input effective VSWR _{7ei}			1.261	1.248	1.238	1.229	1.221		
83										
84	Pad e to Pad b Ripple			0.79	0.79	0.78	0.78	0.77 dB		
85										
86	Pad e Output equiv gamma _{7eo}			0.137	0.136	0.135	0.134	0.134		
87	Pad e Output equiv VSWR _{7eo}			1.317	1.314	1.312	1.310	1.308		
88	Pad e Output effective VSWR _{7eo}			1.33	1.33	1.33	1.33	1.33		
89	Pad e Integrated Output Power P _{7o}									-23.6 dBm
90	Pad e Output Power P _{7o}			-36.1	-31.2	-28.2	-29.3	-28.3 dBm		
91	Pad e Loss L _e	0.0 dB		0.0	0.0	0.0	0.0	0.0 dB		
92	Pad e Input effective NT _{8ei}			19,340	19,642	19,900	20,130	20,341 K		
93	Pad e Input effective VSWR _{8ei}			1.261	1.248	1.238	1.229	1.221		
94										
95	Amp C Output VSWR _{Co}	1.33		1.33	1.33	1.33	1.33	1.33		
96	Amp C Integrated Output Power P _{Co}								Total Cold Cartridge Power ->	-23.6 dBm
97	Amp C Output Power P _{Co}			-36.1	-31.2	-28.2	-29.3	-28.3 dBm		
98	Amp C Gain (Warm IF Amp)			22	25	28	31	34		
99	Amp C NT (NF Warm IF Amp)	2.0 dB		170	170	170	170	170 K		
100	Amp C Input effective NT _{Cei}			292	232	201	186	178 K		
101	Amp C Input VSWR _{Ci}	1.8		1.80	1.80	1.80	1.80	1.80		
102										
103	Pad f Ouput effective VSWR _{9eo}			1.665	1.652	1.641	1.632	1.624		
104	Pad f Integrated Output Power P _{9o}									-51.7 dBm
105	Pad f Output Power P _{9o}			-58.1	-56.2	-56.2	-60.3	-62.3 dBm		
106	Pad f Loss L _f	0.0 dB		0.0	0.0	0.0	0.0	0.0 dB		
107	Pad f Input effective NT _{10ei}			292	232	201	186	178 K		
108	Pad f Input effective VSWR _{10ei}			1.80	1.80	1.80	1.80	1.80		
109	Pad f Input equiv. VSWR _{10ei}			1.76	1.76	1.75	1.74	1.74		
110	Pad f Input equiv gamma _{10ei}			0.277	0.275	0.273	0.271	0.270		
111										

Table 3: Spreadsheet 2

	A	B	C	D	E	F	G	H	I	J	
112	Cold Cartridge Gain			22.7	24.7	24.6	20.6	18.5 dB			
113											
114	Cable g Output effective VSWR 10eo			1.66	1.65	1.64	1.63	1.62			
115	Cable g Integrated Output Power P 10o									-51.7 dBm	
116	Cable g Output Power P 10o			-58.1	-56.2	-56.2	-60.3	-62.3 dBm			
117	Cable g Loss Lg			0.28	0.35	0.40	0.45	0.49 dB			
118	at freq			76.2 dB per 100 ft							
119	Cable g length			18.0 GHz							
120	Cable g NT g			0.24 m							
121	Cable g Input effective NT 11ei			1.0	1.2	1.4	1.5	1.7 K			
122	Cable g Input effective VSWR 11ei			312	252	222	207	201 K			
123				1.731	1.717	1.705	1.695	1.685			
124	Amp D/Pad h to Pad f/Amp C Ripple			1.24	1.22	1.21	1.19	1.18 dB			
125											
126	Pad h Output equiv. gamma 11eo			0.258	0.256	0.254	0.253	0.252			
127	Pad h Output equiv. VSWR 11eo			1.694	1.688	1.682	1.677	1.673			
128	Pad h Output effective VSWR 11eo			1.73	1.73	1.73	1.73	1.73			
129	Pad h Integrated Output Power P 11o									-51.3 dBm	
130	Pad h Output Power P 11o			-57.8	-55.8	-55.8	-59.8	-61.8 dBm			
131	Pad h Loss Lh			2.0 dB							
132	Pad h Input effective NT 12ei			497	402	354	331	320 K			
133	Pad h Input effective VSWR 12ei			1.731	1.717	1.705	1.695	1.685			
134											
135	Amp D Output VSWR Do			2.46							
136	Amp D Integrated Output Power P Do									-49.3 dBm	
137	Amp D Output Power P Do			-55.8	-53.8	-53.8	-57.8	-59.8 dBm			
138	Amp D Gain G D			dB							
139	Amp D NT D			83 K							
140	Amp D Input effective NT Dei			136	83	83	83	136 K			
141				137.6	83.8	83.7	84.7	138.5 K			

Table 4: Spreadsheet 3

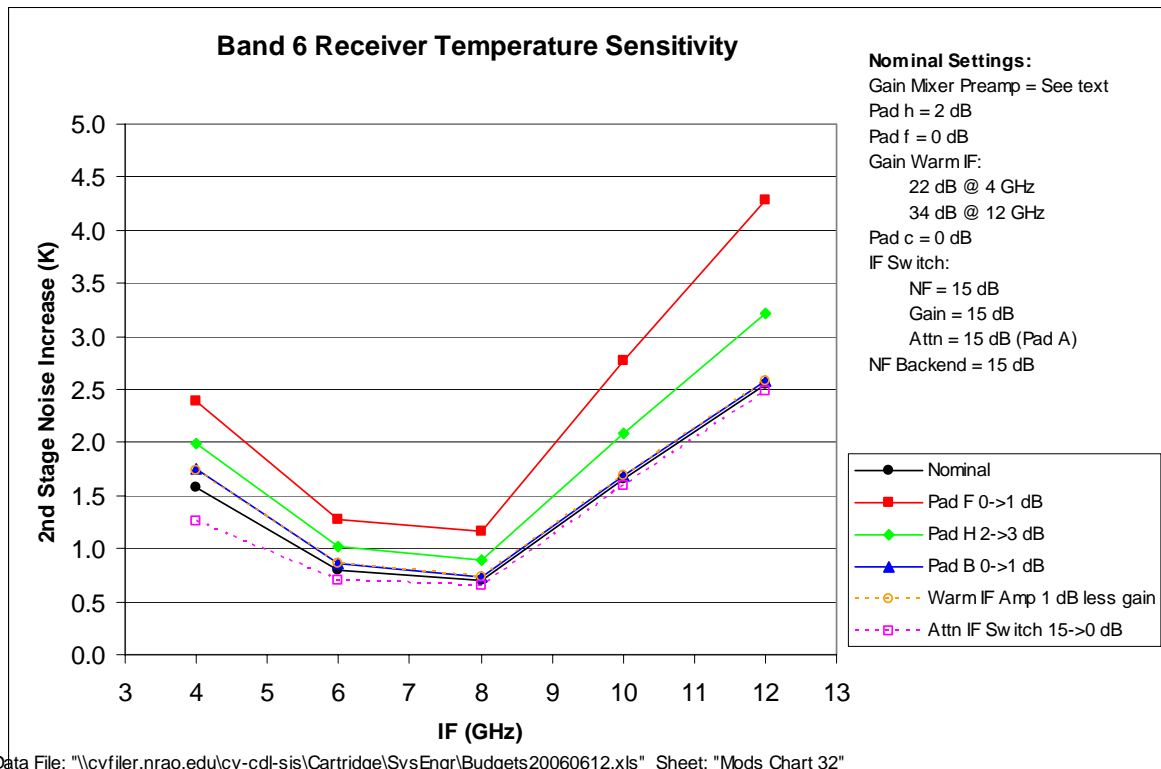


Figure 3: Receiver Temperature Sensitivity